

**AMENDMENTS TO THE CLAIMS**

**This listing of claims will replace all prior versions and listings of claims in the application:**

**LISTING OF CLAIMS:**

1. (currently amended): A process for producing a cold-rolled ferritic/martensitic dual-phase steel strip, wherein a slab, the chemical composition of which comprises, by weight:

0.010% ≤ C ≤ 100%

0.050% ≤ Mn ≤ 1.0%

0.010% ≤ Cr ≤ 1.0%

0.010% ≤ Si ≤ 0.50%

0.001% ≤ P ≤ 0.20%

0.010% ≤ Al ≤ 0.10%

N ≤ 0.010%

the balance being iron and impurities resulting from the smelting, is hot rolled, said process then comprising:

- coiling the hot-rolled strip obtained at a temperature of between 550 and 850°C;

then

- cold rolling the strip with a reduction ratio of between 60 and 90%; then
- annealing the strip continuously in the intercritical range; and
- cooling it down to the ambient temperature in one or more steps, the cooling

rate between 600°C and the ambient temperature being between 100°C/s and 1500°C/s; and

- optionally tempering it at a temperature below 300°C less than 250°C,

the annealing and cooling operations being carried out in such a way that the strip finally contains from 1 to 15% martensite.

2. (original): The process as claimed in claim 1, wherein the chemical composition of the steel comprises:

0.020% ≤ C ≤ 0.060%

0.300% ≤ Mn ≤ 0.500%

0.010% ≤ Cr ≤ 1.0%

0.010% ≤ Si ≤ 0.50%

0.010% ≤ P ≤ 0.100%

0.010% ≤ Al ≤ 0.10%

N ≤ 0.010%

the balance being iron and impurities resulting from the smelting.

3. (previously presented): The process as claimed in claim 1, wherein the strip is hot rolled at a temperature above 850°C.

4. (previously presented): The process as claimed in claim 1, wherein the strip is hot rolled at a temperature of between 550 and 750°C.

5. (previously presented): The process as claimed in claim 1, wherein the strip is cold rolled with a reduction ratio of between 70 and 80%.

6. (previously presented): The process as claimed in claim 1, wherein the continuous annealing of the cold-rolled strip comprises a temperature rise phase followed by a soak phase at a predetermined temperature.

7. (original): The process as claimed in claim 6, wherein the soak temperature is between Ac<sub>1</sub> and 900°C.

8. (original): The process as claimed in claim 7, wherein the soak temperature is between 750 and 850°C.

9. (previously presented): The process as claimed in claim 1, wherein the cooling down

to the ambient temperature comprises a first, slow cooling step between the soak temperature and 600°C, during which the cooling rate is less than 50°C/s, followed by a second cooling step at a higher rate, of between 100°C/s and 1500°C/s, down to the ambient temperature.

10. (original): The process as claimed in claim 9, wherein the second cooling step is carried out by water quenching.

11. (previously presented): The process as claimed in claim 1, wherein the cooling is carried out in a single operation at a cooling rate of between 100°C/s and 1500°C/s.

12. (original): The process as claimed in claim 11, wherein the cooling is carried out by water quenching.

13. (withdrawn): A cold-rolled ferritic/martensitic dual-phase steel strip, the chemical composition of which comprises, by weight:

0.010% ≤ C ≤ 100%

0.050% ≤ Mn ≤ 1.0%

0.010% ≤ Cr ≤ 1.0%

0.010% ≤ Si ≤ 0.50%

0.001% ≤ P ≤ 0.20%

0.010% ≤ Al ≤ 0.10%

N ≤ 0.010%

the balance being iron and impurities resulting from the smelting, the strip furthermore containing between 1% and 15% martensite.

14. (withdrawn): The steel strip as claimed in claim 13, the chemical composition of which furthermore comprises:

0.020% ≤ C ≤ 0.060%

0.300% ≤ Mn ≤ 0.500%

0.010% ≤ Cr ≤ 1.0%

0.010% ≤ Si ≤ 0.50%

0.010% ≤ P ≤ 0.100%

0.010% ≤ Al ≤ 0.10%

N ≤ 0.010%

the balance being iron and impurities resulting from the smelting.

15. (withdrawn): The steel strip as claimed in either of claims 13 and 14, which has a tensile strength  $R_m$  of greater than 450 MPa.

16. (withdrawn): The steel strip as claimed in claim 15, which has a tensile strength  $R_m$  of greater than 500 MPa.

17. (withdrawn ): The steel strip as claimed in claim 16, further which has a tensile strength  $R_m$  of greater than 600 MPa.

18. (withdrawn): The steel strip as claimed in any one of claims 13 to 17, which has a mean anisotropy coefficient  $r$  of greater than 1.1.

19. (withdrawn): The steel strip as claimed in claim 18, further which has a mean anisotropy coefficient  $r$  of greater than 1.3.

20. (withdrawn): The steel strip as claimed in any one of claims 13 to 19, which furthermore contains between 1% and 10% martensite.

21. (withdrawn): The steel strip as claimed in claim 20, which furthermore contains between 5% and 8% martensite.

22. (withdrawn): The use of a steel strip as claimed in any one of claims 13 to 21 for the production of automobile parts by deep drawing.